

.PROCESS CALCULATIONS FOR 92 MLD STP AT UJJAIN							
1	DESIGN BASIS						
1.1	FLOW						
	Average Flow		=	92	MLD		
			=	3833.33	m ³ /hr		
			=	1.06	m ³ /s		
	Peak Factor		=	2			
	Peak Flow		=	184	MLD		
			=	7666.67	m ³ /hr		
			=	2.13	m ³ /s		
1.2	DESIGN QUALITY OF RAW SEWAGE						
	BOD5		=	100	mg/l		
	COD		=	250	mg/l		
	TSS		=	200	mg/l		
	TKN (as N)		=	20	mg/l		
	TP (as PO ₄)		=	5	mg/l		
1.3	DESIGN QUALITY OF TREATED SEWAGE						
	oBOD5 @ 20 C		≤	10	mg/l		
	COD		≤	50	mg/l		
	TSS		≤	10	mg/l		
	TN (as N)		≤	10	mg/l		
	TP (as PO ₄)		≤	2	mg/l		
2	RAW SEWAGE PUMPING STATION						
2.1	RECEIVING CHAMBER						
	No. of Units		=	1	No.		
	Design Flow		=	Peak Flow			
			=	184	MLD		
			=	7666.67	m ³ /hr		
			=	2.13	m ³ /sec		
	Hydraulic Retention Time (HRT) at Peak Flow		=	30	sec		
	Volume required		=	2.40 x 30			
			=	63.88888889	m ³		
	Side Water Depth (SWD) provided		=	2.5	m		
	Width provided		=	6	m		
	Length provided		=	6	m		
	Freeboard provided		=	0.5	m		
	Volume provided		=	90	m ³		
	Size of Receiving Chamber = 1 unit x 6 m x 6 m x 2.5 m						
2.2	COARSE SCREEN CHANNELS						
	No. of Mechanical (Working) Screens		=	2	Nos.		
	No. of Manual (Standby) Screens		=	1	Nos.		
	Total No. of Screens		=	3			
2.2.1	COARSE SCREEN CHANNEL: MECHANICAL						
	No. of Mechanical Screens		=	2	Nos.		
	Design Flow		=	Peak Flow			
			=	184	MLD		
			=	7666.67	m ³ /hr		
			=	2.13	m ³ /sec		
	Average Flow		=	92	MLD		
			=	3833.33	m ³ /hr		
			=	1.06	m ³ /sec		

Design Flow in each Screen	=	2.13	m ³ /sec		
		2	No.		
	=	1.064814815	m ³ /sec		
Average Flow in each Screen	=	1.06	m ³ /sec		
		2	No.		
	=	0.532407407	m ³ /sec		
Maximum Velocity through Screen at PeakFlow	=	1.0	m/sec		
Minimum Velocity through Screen at AverageFlow	=	0.6	m/sec		
Clear Area of Opening through Screen at PeakFlow	=	1.064814815	m ³ /sec		
		1.0	m/sec		
	=	1.064814815	m ²		
Clear Area of Opening through Screen atAverage Flow	=	0.532407407	m ³ /sec		
		0.6	m/sec		
	=	0.887345679	m ²		
Considering maximum Area of Opening through Screen	=	1.064814815	m ²		
Clear Spacing of Bars	=	20	mm		
Thickness of Bars	=	10	mm		
Gross Area of Screen	=	1.197 x (20+10) / 20			
	=	1.597222222	m ²		
Assuming Depth of Screen Channel	=	1.6	m		
Gross Width of Screen	=	1.796 / 1.6			
	=	0.998263889	m		
No. of Bars	=	(Gross Width of Screen / Center to Center Spacing of Bars) - 1			
	=	(1.123 / ((20 + 10)/1000) - 1			
	=	32.27546296	Nos.		
Say	=	33	Nos.		
Width of Screen provided	=	(Number of Bars+1) x Clear Spacing + (Number of Bars x Bar Thickness)			
	=	1010	mm		
Say	=	1100	mm		
Width of Side Frame provided	=	150	mm		
Width of Screen Channel provided	=	1300	mm		
Height of Blind Plate provided at bottom of the Screen	=	50	mm		
Liquid Depth of Screen Channel provided	=	1650	mm		
Length of Screen Channel provided	=	6000	mm		
Freeboard provided	=	300	mm		
Head Loss across Screen	=				
Head Loss across Screen	=	0.0728 (V ₂ - v ₂)			
V = Velocity through Screen at Peak Flow	=	Peak Flow through Screen Channel / Clear Area of Opening through Screen			
	=	1			
v = Velocity in approach Channel at Peak Flow	=	Peak Flow through Screen Channel / Cross Sectional Area of Screen Channel			

			=	0.67			
	Head Loss across Screen at Peak Flow		=	0.040			
	Head Loss across Screen at 50% CloggedCondition						
	Velocity through Screen at 50% CloggedCondition at Peak Flow		=	1.918			
	Head Loss across screen at 50% CloggedCondition at Peak Flow		=	0.249			
			<	0.3	m/sec		OK
	Size of Mechanical Coarse Screens = 2 units x6 m x 1.4 m x 1.65 m						
2.2.2	COARSE SCREEN CHANNEL: MANUAL						
	No. of Manual Screen		=	1	No.		
	Design Flow		=	1/2Peak flow			
			=	92	MLD		
			=	3833.333333	m3/hr		
			=	1.06481	m3/sec		
	Average Flow		=	46	MLD		
			=	1916.667	m3/hr		
			=	0.532	m3/sec		
	Design Flow in each Screen		=	1.06481	m3/sec		
				1	No.		
			=	1.064814815	m3/sec		
	Average Flow in each Screen		=	0.532	m3/sec		
				1	No.		
			=	0.532407407	m3/sec		
	Maximum Velocity through Screen at PeakFlow		=	1.0	m/sec		
	Minimum Velocity through Screen at AverageFlow		=	0.6	m/sec		
	Clear Area of Opening through Screen forPeak Flow		=	1.064814815	m3/sec		
				1.0	m/sec		
			=	1.064814815	m2		
	Clear Area of Opening through Screen forAverage Flow		=	0.532407407	m3/sec		
				0.6	m/sec		
			=	0.887345679	m2		
	Considering maximum Area of Opening through Screen		=	1.064814815	m2		
	Clear Spacing of Bars		=	20	mm		
	Thickness of Bars		=	10	mm		
	Gross Area of Screen		=	1.197 x (20+10) / 20			
			=	1.597222222	m2		
	Assuming Depth of Screen Channel		=	1.65	m		
	Gross Width of Screen		=	0.968013468	m		
	No. of Bars		=	(Gross Width of Screen / Center to Center Spacing of Bars) - 1			
			=	(1.089 / ((20 + 10)/1000) - 1			
			=	31.2671156	Nos.		
	Say		=	32	Nos.		

	Width of Screen provided	=	(Number of Bars+1) x Clear Spacing + (Number of Bars x Bar Thickness)		
		=	(50+1) x 20 + (50 x 10)		
		=	980	mm	
	Say	=	980	mm	
	Width of Side Frame provided	=	50	mm	
	Width of Screen Channel	=	1080	mm	
	Liquid Depth of Screen Channel provided	=	1650	mm	
	Length of Screen Channel provided	=	6000	mm	
	Freeboard provided	=	300	mm	
	Head Loss across Screen	=			
	Head Loss across Screen	=	0.0728	(V2 - v2)	
	V = Velocity through Screen at Peak Flow	=	Peak Flow through Screen Channel / Clear Area of Opening through Screen		
		=	1		
	v = Velocity in approach Channel at Peak Flow	=	Peak Flow through Screen Channel / Cross		
	Head Loss across Screen at Peak Flow	=	0.667		
	Head Loss across Screen at 50% Clogged condition	=	3-4	m/km	
	Head Loss across Screen at 50% CloggedCondition	=			
	Velocity through Screen at 50% CloggedCondition at Peak Flow	=	1.532		
	Head Loss across screen at 50% CloggedCondition at Peak Flow	=	0.152		
		<	0.3	m/sec	OK
	Size of Manual Coarse Screens = 1 unit x 7 m x 1.7m x 1.65 m				
2.3 RAW SEWAGE SUMP (WET WELL) OF RAW SEWAGE PUMPING STATION					
	No. of Units	=	1	No.	
	Average Flow	=	92	MLD	
		=	3833.33	m3/hr	
		=	1.0648	m3/sec	
	Design Flow	=	Peak Flow		
		=	207	MLD	
		=	8625.00	m3/hr	
		=	2.3958	m3/sec	
	Hydraulic Retention Time (HRT) at Peak Flow	=	5	min	
	Volume required	=	718.75	m3	
	Hydraulic Retention Time (HRT) at AverageFlow	=	Volume / Average Flow		
		=	7.8125	min	
		<	30	min	OK
	Volume of Receiving Chamber (Inside WetWell)	=	0	m3	
	Total Volume of Wet Well	=	718.75	m3	
	Side Water Depth (SWD) provided	=	3.5	m	
	Plan Area of Wet Well	=	205.3571429	m2	
	Diameter of Sump required	=	16.1740983	m	
	Diameter of Sump provided	=	17	m	
	Freeboard provided	=	0.5	m	
	Volume of Sump provided	=	821.43	m3	
	Size of Wet Well = 1 unit x 17 m Dia x 3.5 m SWD				
2.4 RAW SEWAGE TRANSFER PUMPS					
	Present Average Flow (DWF)	=	4583	m3/hr	
	Half Present Average Flow (1/2 DWF)	=	2292	m3/hr	
	Present Peak Flow (WWF)	=	10313	m3/hr	
	Pump Capacity provided	=			
I	1 DWF: 3 Nos.	=	2063	m3/hr	

	No. of Working Pumps	=	5	No.	
	No. of Standby Pumps	=	2	No.	
	Head Provided	=	20	m	
	3 PRIMARY TREATMENT UNITS				
	3.1 INLET CHAMBER				
	No. of Units	=	1	No.	
	Design Flow	=	Peak Flow		
	Peak Flow	=	207	MLD	
		=	8625	m ³ /hr	
		=	2.40	m ³ /sec	
	Hydraulic Retention Time (HRT) at Peak Flow	=	30	sec	
	Volume required	=	2.4 x 30		
		=	71.875	m ³	
	Side Water Depth (SWD) provided	=	2.5	m	
	Width provided	=	6	m	
	Length provided	=	6	m	
	Freeboard provided	=	0.5	m	
	Volume provided	=	90	m ³	
	Size of Inlet Chamber = 1 unit x 6 m x 6m x 2.5 m				
	3.2 FINE SCREEN CHANNELS				
	No. of Mechanical (Working) Screens	=	2	Nos.	
	No. of manual (Standby) Screens	=	1	Nos.	
	Total No. of Screens	=	3		
	3.2.1 FINE SCREEN CHANNELS: MECHANICAL				
	No. of Mechanical Screens	=	2	Nos.	
	Design Flow	=	Peak Flow		
		=	207	MLD	
		=	8625	m ³ /hr	
		=	2.40	m ³ /sec	
	Average Flow	=	92	MLD	
		=	3833.33	m ³ /hr	
		=	1.0648	m ³ /sec	
	Design Flow in each Screen	=	2.40	m ³ /sec	
			2	No.	
		=	1.197916667	m ³ /sec	
	Average Flow in each Screen	=	1.0648	m ³ /sec	
			2	No.	
		=	0.532407407	m ³ /sec	
	Maximum Velocity through Screen at PeakFlow	=	1.0	m/sec	
	Minimum Velocity through Screen at AverageFlow	=	0.6	m/sec	
	Clear Area of Opening through Screen at PeakFlow	=	1.197916667	m ³ /sec	
			1.0	m/sec	
		=	1.197916667	m ²	
	Clear Area of Opening through Screen atAverage Flow	=	0.532407407	m ³ /sec	
			0.6	m/sec	

			=	0.887345679	m ²		
	Considering maximum Area of Opening through Screen		=	1.197916667	m ²		
	Clear Spacing of Bars		=	6	mm		
	Thickness of Bars		=	2	mm		
	Gross Area of Screen		=	1.432 x (6+2) /6			
			=	1.597222222	m ²		
	Assuming Depth of Screen Channel		=	1.5	m		
	Gross Width of Screen						
			=	1.064814815	m		
	No. of Bars		=	(Gross Width of Screen / Center to Center Spacing of Bars) - 1			
			=	(1.273 / ((6 + 2)/1000)) - 1			
			=	132.1018519	Nos.		
	Say		=	133	Nos.		
	Width of Screen provided		=	(Number of Bars+1) x Clear Spacing + (Number of Bars x Bar Thickness)			
			=	(159+1) x 6 + (159 x 2)			
			=	1278	mm		
	Say		=	1300	mm		
	Width of Side Frame provided		=	150	mm		
	Width of Screen Channel provided		=	1600	mm		
	Height of Blind Plate at Bottom of Screen provided		=	50	mm		
	Liquid Depth of Screen Channel provided		=	1550	mm		
	Length of Screen Channel provided		=	8000	mm		
	Freeboard provided		=	300	mm		
	Head Loss across Screen						
	Head Loss across Screen		=	0.0728 (V ₂ - v ₂)			
	V = Velocity through Screen at Peak Flow		=	Peak Flow through Screen Channel / Clear Area of Opening through Screen			
			=	0.979			
	v = Velocity in approach Channel at Peak Flow		=	Peak Flow through Screen Channel / Cross Sectional Area of Screen Channel			
			=	0.578			
	Head Loss across Screen at Peak Flow		=	0.046			
	Head Loss across Screen at 50% CloggedCondition						
	Velocity through Screen at 50% CloggedCondition at Peak Flow		=	1.959			
	Head Loss across screen at 50% CloggedCondition at Peak Flow		=	0.255			
			<	0.3	m/sec		OK
	Size of Mechanical Fine Screens = 2 units x 8 m x 1.6 m x 1.55 m						
3.2.2	FINE SCREEN CHANNELS: MANUAL						
	No. of Manual Screen		=	1	No.		
	Design Flow		=	1/2Peak Flow			
			=	103.5	MLD		
			=	4312.5	m ³ /hr		
			=	1.197916667	m ³ /sec		
	Average Flow		=	46	MLD		
			=	1916.666667	m ³ /hr		
			=	0.532407407	m ³ /sec		
	Design Flow in each Screen		=	1.197916667	m ³ /sec		
				1	No.		
			=	1.197916667	m ³ /sec		

Average Flow in each Screen	=	0.532407407	m3/sec		
		1	No.		
	=	0.532407407	m3/sec		
Maximum Velocity through Screen at PeakFlow	=	1.0	m/sec		
Minimum Velocity through Screen at AverageFlow	=	0.6	m/sec		
Clear Area of Opening through Screen forPeak Flow	=	1.197916667	m3/sec		
		1.0	m/sec		
	=	1.197916667	m2		
Clear Area of Opening through Screen forAverage Flow	=	0.532407407	m3/sec		
		0.6	m/sec		
	=	0.887345679	m2		
Considering maximum Area of Opening through Screen	=	1.197916667	m2		
Clear Spacing of Bars	=	10	mm		
Thickness of Bars	=	3	mm		
Gross Area of Screen	=	$1.432 \times (10+3) / 10$			
	=	1.557291667	m2		
Assuming Depth of Screen Channel	=	1.55	m		
Gross Width of Screen	=	1.004704301	m		
No. of Bars	=	(Gross Width of Screen / Center to Center)			
	=	$(1.201 / ((10 + 3)/1000)) - 1$			
	=	76.28494624	Nos.		
Say	=	77	Nos.		
Width of Screen provided	=	(Number of Bars+1) x Clear Spacing + (Number of Bars x Bar Thickness)			
	=	$(113+1) \times 10 + (113 \times 3)$			
	=	1011	mm		
Say	=	1011	mm		
Width of Side Frame provided	=	50	mm		
Width of Screen Channel	=	1600	mm		
Width of Screen Channel Provided	=	1600			
Liquid Depth of Screen Channel provided	=	1550	mm		
Length of Screen Channel provided	=	8000	mm		
Freeboard provided	=	300	mm		
Head Loss across Screen					
Head Loss across Screen	=	0.0728	$(V_2 - v_2)$		
V = Velocity through Screen at Peak Flow	=	Peak Flow through Screen Channel / Clear Area of Opening through Screen			
	=	0.751			
v = Velocity in approach Channel at Peak Flow	=	Peak Flow through Screen Channel / Cross Sectional Area of Screen Channel			
Head Loss across Screen at Peak Flow	=	0.578			
Head Loss across Screen at 50% Clogged condition	=	0.017			
Head Loss across Screen at 50% CloggedCondition					
Velocity through Screen at 50% CloggedCondition at Peak Flow	=	1.502			
Head Loss across screen at 50% CloggedCondition at Peak Flow	=	0.140			
	<	0.3	m/sec		OK
Size of Manual Fine Screens = 1 unit x 8 m x 1.6 m x 1.55 m					
3.3 GRIT CHAMBERS					

	No. of Working Units	=	2	Mechanical	
	No. of Standby Units	=	0	Manual	
	Total No. of Units	=	2	Nos	
3.3.1	GRIT CHAMBER: MECHANICAL				
	No. of Mechanical Grit Chamber	=	2		
	Design Flow	=	Peak Flow		
	Peak Flow	=	184	MLD	
		=	184000	m ³ /day	
		=	7666.666667	m ³ /hr	
		=	2.12962963	m ³ /sec	
	Design Flow to each Grit Chamber				
		=	92000	m ³ /day	
		=	3833.333333	m ³ /hr	
		=	1.064814815	m ³ /sec	
According to "Manual on Sewerage & Sewage Treatment" published by Central Public Health and Environmental Engineering Organisation (CPHEEO),					
	Surface Overflow Rate for 0.15 mm dia. Particle Size with Specific G	=	1555	m ³ /m ² /day	
	Considering Design Overflow Rate	=	960	m ³ /m ² /day	
	Area of Grit Chamber required	=	123750	m ³ /day	
		=	960	m ³ /m ² /day	
		=	128.91	m ²	
	Square Side of Grit Chamber required	=	128.91		
		=	11.35	m	
	Length of Chamber provided	=	11.5	m	
	Width of Chamber provided	=	11.5	m	
	Hydraulic Retention Time (HRT) in Grit Chamber at Peak Flow	=	60	sec	
	Volume of Grit Chamber required	=	1.432 x 60		
		=	85.938	m ³	
	Depth required in Grit Chamber	=	85.938 / (11.5 x 11.5)		
		=	0.65	m	
	Say	=	0.65	m	
	Grit Storage Depth	=	0.25	m	
	Total Liquid Depth required	=	0.9	m	
	Total Liquid Depth provided	=	0.9		
	Freeboard provided	=	0.3	m	
	Size of Grit Chambers = 2 units x 11.5m x 11.5 m x 0.9 m				
4 PROCESS DESIGN FOR SBR BASINS					
4.1 TREATMENT SEQUENCE					
A	Sewage to be treated in a day	=	92000	m ³	
B	Time for "Fill & Aerate" phase provided	=	2	hrs	
C	Time for "Settle" phase provided	=	1	hrs	
D	Time for "Decant" phase provided	=	1	hrs	
E	Total Cycle Time provided = B + C + D	=	4	hrs	
F	No. of Cycles provided per Basin per day= 24 / E	=	6	Nos.	
G	Aeration Time provided per Basin per day= B x F	=	12	hrs	
H	No. of Basins under "Fill" simultaneously	=	3	Nos.	

I	No. of Basins under "Aerate" simultaneously	=	3	Nos.	
J	No. of Basins under "Decant" simultaneously	=	2	Nos.	
K	Flow Rate = A / 24	=	3833.333333	m ³ /hr	
L	Flow Rate to each Basin = K / H	=	1277.777778	m ³ /hr	
4.2 BASIN SIZING					
A	Volume of Sewage to be treated in day	=	92000	m ³ /day	
B	Inlet BOD	=	100	mg/l	
C	MLSS considered	=	4300	mg/l	
D	MLVSS = MLSS x 0.7	=	3010	mg/l	
E	F/M considered	=	0.08		
F	Total Volume of Aeration Basins required= (A x B) / (D x E)	=	38205.98	m ³	
G	No. of Basins provided	=	6	Nos.	
H	Volume required per Basin = F / G	=	6367.663344	m ³	
I	Side Water Depth (SWD) provided	=	5.5	m	
J	Width provided	=	31.0	m	
K	Length required	=	37.3	m	
L	Length provided	=	38.0	m	
M	Volume provided = I x J x L	=	6479	m ³	
N	Total Volume provided = M x G	=	38874	m ³	
O	Freeboard provided	=	0.5	m	
P	Total Depth provided = I + O	=	6	m	
Q	Hydraulic Retention Time (HRT) provided= N x 24 / A	=	10.14	hrs	
R	Solids Retention Time (SRT) provided = (N x C) / (Excess Sludge x 1000)	=	55.53428571	days	
S	Recirculation Ratio provided	=	25%	Flow per	
T	Feed Flow to each Basin	=	1277.777778	m ³ /hr	
U	Recirculation Flow required = T x S	=	319.4444444	m ³ /hr	
V	Capacity of Return Activated Sludge (RAS) Pump provided	=	320	m ³ /hr	
Size of SBR Basins = 6 units x 61.7 m x 31 m x 5.5 m					
4.3 SELECTOR ZONE					
A	Design Flow = Feed Flow + Recirculation Flow	=	1597.222222	m ³ /hr	
B	Hydraulic Retention Time (HRT) provided at Design Flow	=	55	min	
C	Volume required = (A x B) / 60	=	1464.12037	m ³	
D	No. of Sub-Compartments provided per Basin	=	6	No.	
E	Side Water Depth (SWD) provided	=	5.5	m	
F	Length provided	=	31	m	
G	Width required = C / (F x E)	=	8.587216249	m	
H	Width provided	=	9	m	
I	Volume provided = F x H x E	=	1534.5	m ³	
4.4 ACTUAL OXYGEN REQUIREMENT (AOR) CALCULATIONS					
A	Volume of Sewage to be treated in day	=	92000	m ³	
B	Inlet BOD ₅	=	100	mg/l	
C	Outlet BOD ₅	=	10	mg/l	
D	BOD ₅ removed = C - D	=	90	mg/l	
E	BOD ₅ removed in a day = A x D / 1000	=	8280	Kg/day	
F	O ₂ required for oxidation of BOD	=	1.2	Kg/Kg BOD	
G	O ₂ required for oxidation of BOD = E x F	=	9936	Kg/day	
H	Inlet TKN	=	20	mg/l	
I	Outlet NH ₃ -N	=	1	mg/l	
J	Nitrogen assimilated during oxidation of BOD= D x 5%	=	4.5	mg/l	
K	NH ₃ -N nitrified in a day = H - I - J	=	14.5	mg/l	
L	NH ₃ -N nitrified in a day = A x K / 1000	=	1334	Kg/day	
M	O ₂ required for nitrification of NH ₃ -N	=	4.56	Kg/NH ₃ -N	
N	O ₂ required for nitrification of NH ₃ -N = L x M	=	6083.04	Kg/day	II

O	NO ₃ -N generated assuming 75% nitrification of NH ₃ -N = K x 75%	=	10.875	mg/l		
P	Outlet NO ₃ -N	=	3	mg/l		
Q	NO ₃ -N that is denitrified= O – P	=	7.875	Kg/day		
R	Amount of NO ₃ -N that is denitrified= A x Q / 1000	=	724.5	Kg/day		
S	O ₂ credit during de-nitrification of NO ₃ -N	=	2.86	Kg/Kg NO ₃ -		
T	O ₂ credit available during de-nitrification	=	6,548	Kg/day		III
W	Total O ₂ required including O ₂ credit during de-nitrification = G + N – T	=	9471.04	Kg/day		
4.5	STANDARD OXYGEN REQUIREMENT (SOR) CALCULATIONS					
A	Actual Oxygen Transfer Rate (AOTR) under field conditions	=	9471.04	Kg/day		
B	As per Equation 5-55, Pg No 429, Wastewater Engineering - Treatment and Reuse, Metcalf & Eddy..... Standard Oxygen Transfer Rate (SOTR) in Tap Water at 200 C and Zero Dissolved Oxygen: AOTR ÷ [((βC'S,T,H – CL) ÷ CS,20) x 1.024(T – 20) x α x F]					
	Where,					
	AOTR = Actual Oxygen Transfer Rate under field conditions	=	9471.04	Kg/day		
	As per Pg No 429, Wastewater Engineering - Treatment and Reuse, Metcalf & Eddy..... C' : Average Dissolved Oxygen Saturation Concentration in Clean Water in Aeration Tank at Temperature 'T' and Altitude 'H' S,T,H = CS,T,H x (1/2) x ((Pd / Patm,H)+Ot/21))					
T = Field Temperature	=		27			
H = Altitude of Site	=		527			
	As per Equation B-2, Pg No 1738, Wastewater Engineering - Treatment and Reuse, Metcalf & Eddy..... C = Oxygen Saturation Concentration in Clean Water at Temperature 'T' and Altitude 'H': CS,T,HS,T,H = CS,T x exp(-(g x M x (zb - za)) / (R x T))					
	C = Oxygen Saturation Concentration in Clean Water at Temperature 'T'	=		mg/l		
g = Acceleration due to Grav	=	9.81	m/s ²			
M = Mole of Air	=	28.97	Kg/Kg-			
zb = Elevation (Altitude 'H')	=	527	m			
za = Elevation (Altitude Zero)	=	0	m			
R = Universal Gas Constant	=	8,314	Nm/Kg-mole.K			
T = Temperature	=	300.15	Kelvin			
Hence, CS,T,H	=	7.76	mg/l			
	As per Equation B-2, Pg No 1738, Wastewater Engineering - Treatment and Reuse, Metcalf & Eddy..... Patm,H = PaS,T,H – CL) ÷ C x exp(-(g x M x (zS,20b) x 1.024 - za(T – 20))) / (R x T))					
Pa = Pressure at Zero Altitude	=					
g = Acceleration due to Grav	=	9.81				
M = Mole of Air	=	28.97				
zb = Elevation (Altitude 'H')	=	527	m			
za = Elevation (Altitude Zero)	=	0	m			
R = Universal Gas Constant	=	8,314	Nm/Kg-mole.K			
T = Temperature	=	300.15	Kelvin			
Hence, Patm,H	=	9.54				
	Pd = Pressure at the Depth of Air Release= Patm,H + Effective Aeration					
	Ot = Percentage Oxygen Concentration leaving Tank	=	19.00			18 - 20
	Hence, C'S,T,H	=	9.03	mg/l		
	CL: Operating Oxygen Concentration					
	CS,20: Dissolved Oxygen Saturation Concentration in Clean Water at	=	9.08	mg/l		Table D, Ap
	α: Oxygen Transfer Correction Factor	=	0.65			
	β: Salinity - Surface Tension Correction Factor	=	0.95			
	F: Fouling Factor	=	0.9			
	Hene, SOTR	=	87,369	Kg/day		
C	No. of Basins	=	6	Nos.		
D	Standard O ₂ required at Field Conditions per Basin= B / C	=	1578.506667	Kg/day/Basin		

E	Top Water Level (TWL) in SBR Basins	=	5.5	m		
F	Bottom Water Level (BWL) in SBR Basins	=	3.1	m		
G	Aeration Depth	=	4.3	m		
H	Height at which Diffusers are kept	=	0.25	m		
I	Effective Aeration Depth = G - H	=	4.05	m		
J	SOTE for the above Effective Aeration Depth	=	25.25	%		
K	Fraction of O2 in Air	=	23.18	%		
L	Specific Gravity of Air at Standard Condition	=	1.293			
M	Air required at Field Conditions per Basin= $D / (J \times K \times L)$	=	20858.02009	Nm3/day/Basin		
N	Hours of Aeration per Basin per day	=	12	hr/day/Bas		
O	Air required per hour per Basin = M / N	=	1738.168341	Nm3/hr/Ba sin		
P	No. of Operating Air Blowers per Basin	=	3	Nos.		
Q	Capacity of Air Blowers required = O / P	=	579.389447	Nm3/hr		
R	Capacity of Air Blowers provided	=	5,500	Nm3/hr		
S	Number of Basins per set of Air Blowers	=	2	Nos.		
T	Number of Basins	=	6	Nos.		
U	Number of Operating Air Blowers = P x T / S	=	9	Nos.		
V	Number of Standby Air Blowers(50% of Working Air Blowers)	=	3	Nos.		
4.6 SLUDGE WASTING						
A	Specific Sludge Yield	=	0.81	Kg/Kg BODremoved		
B	BOD removed	=	8280	Kg/day		
C	Excess Sludge to be wasted = B x A	=	6706.8	Kg/day		
D	No. of Basins provided	=	6	Nos.		
E	Sludge to be Wasted per Basin = C / D	=	1117.8	Kg/day		
F	No. of Cycles	=	8	Cycles/day/ Basin		
G	Sludge to be Wasted per Cycle per Basin = E / F	=	139.725	Kg/day		
H	Solids Consistency in the Wasted Sludge	=	0.80%			
I	Volume of Sludge to be Wasted per Cycle perBasin = G / (H x 1000)	=	17.465625	m3		
J	Considering Running Time pf SurplusActivated Sludge (SAS) Pump p	=	10	min		
K	Capacity of SAS Pump required=(I x 60) / J	=	104.79375	m3/hr		
L	Capacity of SAS Pump provided	=	105	m3/hr		
5 DISINFECTION SYSTEM						
5.1 CHLORINE CONTACT TANK						
	No. of Units	=	1	No.		
	Design Flow	=	Average Flow or Decant Flow whichever is more			
	Average Flow	=	3833.33	m3/hr		
	Decant Flow	=	1916.67	m3/hr		
	Hydraulic Retention Time at Average Flow	=	30	min		
	Volume of Chlorine Contact Tank required	=	958.3333333	m3		
	Side Water Depth (SWD) provided	=	3.5	m		
	Width provided	=	8	m		
	Length required	=	34.22619048	m		
	Length provided	=	35	m		
	Volume provided	=	980	m3		
	Freeboard provided	=	0.5	m		
	Size of Chlorination Tank = 1 unit x 35 m x 8m x 3.5 m					
5.2 CHLORINATORS						
	Design Flow	=	Average Flow or Decant Flow whichever is more			
	Average Flow	=	3833.33	m3/hr		
	Decant Flow	=	1916.67	m3/hr		
	Design Chlorine Dosage (Max)	=	4	mg/l		
	Quantity of Chlorine required	=	7.67	Kg/hr		
	No. of Working Chlorinator provided	=	1	No.		
	Capacity of Chlorinator required	=	7.67	Kg/hr		

	Capacity of Chlorinator provided	=	8.00	Kg/hr		
	No. of Standby Chlorinator provided	=	1	No.		
	Quantity of Chlorine required	=	276	Kg/day		
	Considering Storage Period as	=	30	days		
	Quantity of Chlorine required	=	8280	Kg		
	Available Capacity of one Chlorine Tonner	=	928	Kg		
	No. of Chlorine Tonners required	=	8.922413793	Nos.		
	Say	=	9	Nos.		
	No. of Chlorine Tonners in use at any time	=	1	Nos.		
	Total No. of Chlorine Tonners provided	=	10	Nos.		
	6 SLUDGE HANDLING SYSTEM					
	6.1 CENTRIFUGE FEED SUMP					
	Quantity of Sludge to be wasted from SBR Basins	=	6706.8	Kg/day		
	Total Sludge generated	=	6706.8	Kg/day		
	Solids Consistency of Waste Sludge considered	=	0.8%			
	Volume of Sludge to be wasted in a day	=	6706.8 / (0.008 x 1000)			
		=	838.35	m3/day		
		=	34.93	m3/hr		
	Hydraulic Retention Time (HRT) provided in Sludge Sump	=	6.00	hrs		
	Volume of Sludge Sump required	=	209.5875	m3		
	Side Water Depth (SWD) provided	=	3.5	m		
	Width provided	=	7	m		
	Length provided	=	9.00	m		
	Volume provided	=	220.5	m3		
	Freeboard provided	=	0.5	m		
	Size of Centrifuge Feed Pump = 1 unit x 9 m x 7 m x 3.5 m					
	6.2 SLUDGE SUMP AIR BLOWERS					
	Volume of Sludge Sump provided	=	220.5	m3		
	Design Air Agitation Rate	=	1.2	m3/hr/m3		
	Air required for mixing	=	264.6	m3/hr		
	Number of Working Air Blower considered	=	1	No.		
	Capacity of each Air Blower required	=	264.6	m3/hr		
	Capacity of each Air Blower provided	=	265	m3/hr		
	Number of Standby Air Blower provided	=	1	No.		
	Head provided	=	0.4	Kg/cm2		
	6.3 CENTRIFUGE & CENTRIFUGE FEED PUMPS					
	Volume of Sludge to be fed to Centrifuge in a day	=	838.35	m3/day		
	No. of Operating Hours of Centrifuge considered	=	18			
	Capacity of Centrifuge required	=	46.575			
	No. of Working Centrifuge considered	=	4	Nos.		
	Capacity of each Centrifuge required	=	11.64375	m3/hr		
	Capacity of each Centrifuge provided	=	12	m3/hr		
	No. of Standby Centrifuge provided	=	1	No.		
	Capacity of Centrifuge Feed Pump provided	=	12	m3/hr		
	No. of Working Centrifuge Feed Pump provided	=	4	Nos.		
	No. of Standby Centrifuge Feed Pump provided	=	1	No.		
	Head provided	=	15	mWC		
	6.4 POLYELECTROLYTE DOSING SYSTEM					
	Quantity of Sludge to be dewatered in a day	=	6706.8	Kg/day		
	Design Polyelectrolyte Dosage (Max)	=	1.50	Kg/Ton of Dry Solids		
	Quantity of Polyelectrolyte required	=	32.54	Kg/day		
	Design Strength of Polyelectrolyte Solution	=	0.1%			
	Volume of Polyelectrolyte Solution	=	32.54 / (0.001 x 1000)			
		=	32.54	m3		
	No. of Dosing Tanks provided	=	2	Nos.		

Volume of each Dosing Tank required	=	16.27	m ³		
Side Water Depth (SWD) provided	=	2	m		
Length/Width required	=	2.85	m		
Length/Width offered	=	2.85	m		
Volume provided	=	16.27	m ³		
Freeboard provided	=	0.5	m		
Size of Dosing Tanks = 2 units x 2.9 m x 2.9 m x 2.0 m					
No. of Working Polyelectrolyte Dosing Pump provided	=	6	Nos.		
Capacity of each Polyelectrolyte Dosing Pump required	=	Total Volume of Polyelectrolyte Solution / (No. of Dosing Pumps x No. of Hours of			
	=	32.54 / (6 x 18)			
	=	0.301	m ³ /hr		
	=	301	LPH		
Capacity of each Polyelectrolyte Dosing Pump provided	=	410	LPH		
No. of Standby Polyelectrolyte Dosing Pump provided	=	1	No.		